

PID Tuning Rules

File: Ch12_PID_TuningRules.m

Topics:

- * PID Control
- * Gain Margin
- * Tuning Rules

To use the publish function with these notes, be sure you have the displaytable.m from the CBE30338 Utilities folder. Also, please note these notes use the Control Systems Toolbox, and require a reasonably current version of Matlab.

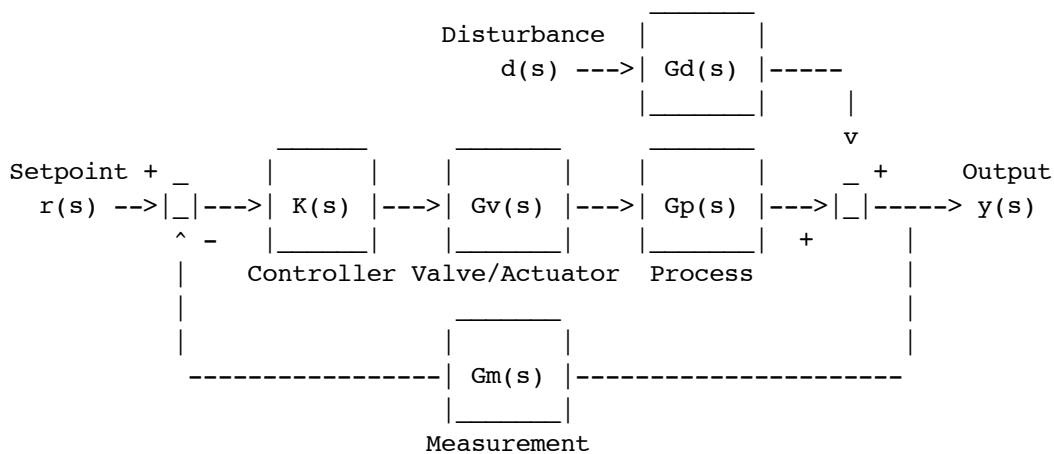
Contents

- [SEMD Example 11.4 with Time Delay](#)
- [Transfer functions](#)
- [Gain Margin](#)
- [Demonstration of the Gain Margin](#)
- [Ziegler-Nichols Tuning Rule: P](#)
- [Ziegler-Nichols Tuning Rule: PI](#)
- [Ziegler-Nichols Tuning Rule: PID](#)
- [Two Degree of Freedom Controller](#)
- [Closed Loop Transfer functions](#)

```
clf;  
clear all;
```

SEMD Example 11.4 with Time Delay

The following diagram shows the basic elements of a feedback control system. The notation follows from Figure 11.8 of the SEMD textbook.



Transfer functions

Process

```
Gp = tf([1],[5 1], 'TimeUnit', 'minutes')
```

Gp =

$$\frac{1}{5s + 1}$$

Continuous-time transfer function.

Disturbance

```
Gd = Gp
```

Gd =

$$\frac{1}{5s + 1}$$

Continuous-time transfer function.

Valve Actuator

```
Gv = tf([1],[2 1], 'TimeUnit', 'minutes')
```

Gv =

$$\frac{1}{2s + 1}$$

Continuous-time transfer function.

Measurement with Time Delay

```
Gm = tf([1],[1 1], 'ioDelay', 1, 'TimeUnit', 'minutes')
```

Gm =

$$\exp(-1*s) * \frac{1}{s + 1}$$

Continuous-time transfer function.

Gain Margin

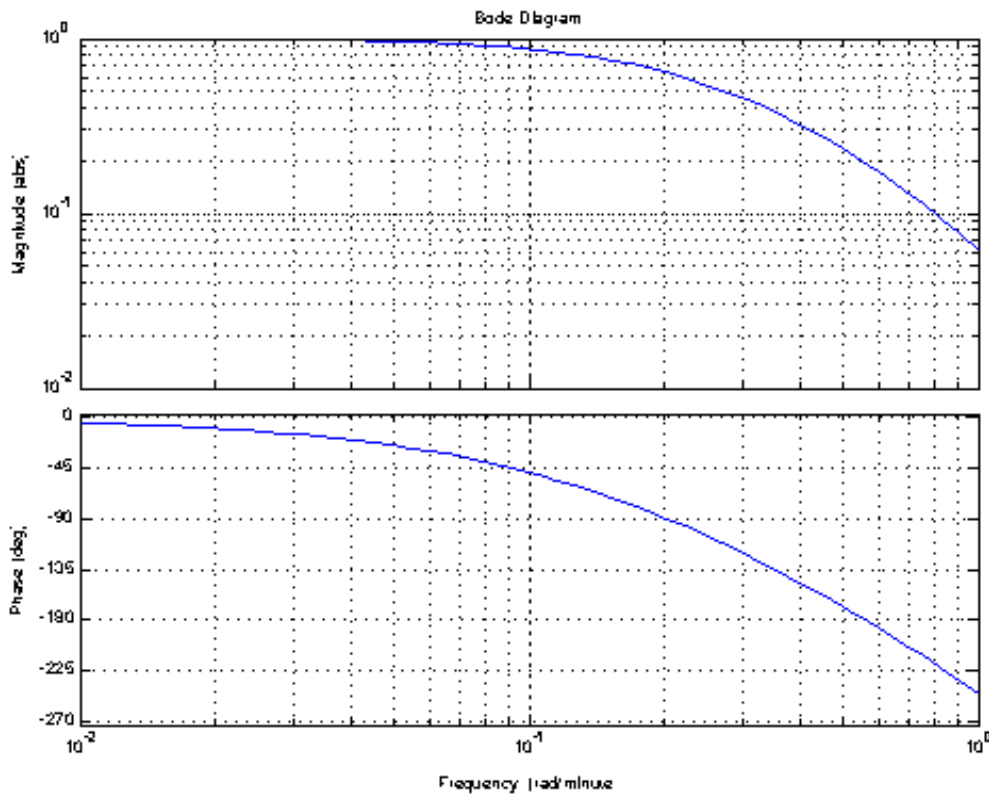
Given the product of transfer functions $G_m*G_p*G_v$, the **gain margin** is the critical value of K_p for which the closed-loop becomes unstable. That critical value is called the 'ultimate gain' K_{cu} .

The gain margin can be found from the Bode plot for $G_m*G_p*G_v$.

```
p = bodeoptions;
p.FreqUnits = 'rad/minute';
p.MagUnits = 'abs';
p.MagScale = 'log';

w = logspace(-2,0);

bodeplot(Gm*Gp*Gv,w,p);
grid;
```



Before going further, use the Bode plot to estimate the cross-over frequency and K_{cu} .

Demonstration of the Gain Margin

The maximum proportional gain is the gain margin. The gain margin and the cross-over frequency can be computed with the Matlab function `margin`.

```
[Kcu,~,wco] = margin(Gm*Gp*Gv);
displaytable([Kcu;wco],{'Gain Margin';'Crossover Freq [rad/min]'});

K = tf([Kcu],[1],'TimeUnit','minutes');

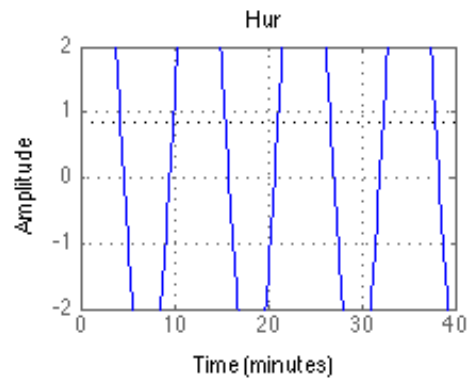
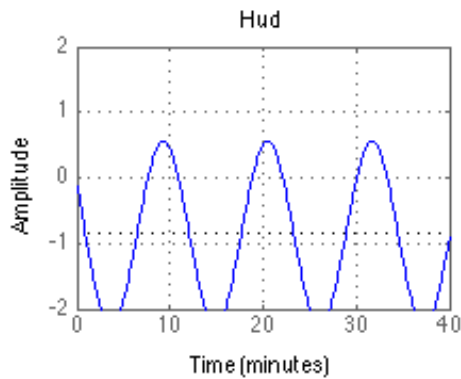
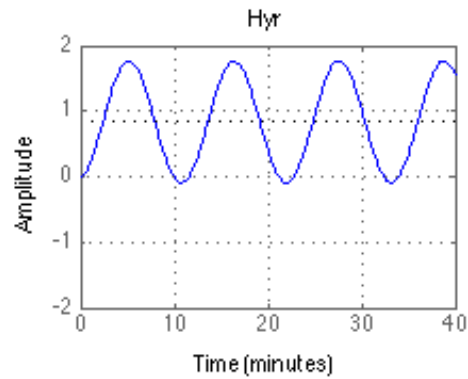
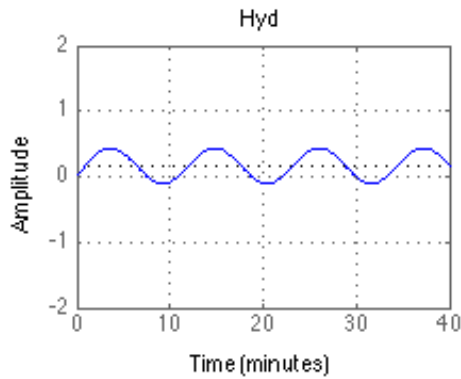
% Closed-loop transfer functions

Hyd = Gd/(1 + Gp*Gv*K*Gm);
Hyr = Gp*Gv*K/(1 + Gp*Gv*K*Gm);
Hud = -K*Gd/(1 + K*Gm*Gp*Gv);
Hur = K/(1 + K*Gm*Gp*Gv);

% Plot Step Responses

t = 0:0.1:40;
ax = [min(t) max(t) -2 2];
subplot(2,2,1);step(Hyd,t);axis(ax);grid;title('Hyd');
subplot(2,2,2);step(Hyr,t);axis(ax);grid;title('Hyr');
subplot(2,2,3);step(Hud,t);axis(ax);grid;title('Hud');
subplot(2,2,4);step(Hur,t);axis(ax);grid;title('Hur');
```

Gain Margin 5.1215
 Crossover Freq [rad/min] 0.56032



Observations

- Marginal stability. Try increasing and decreasing K_p to see what happens.
- Period of Oscillation corresponds to the cross over frequency.

Ziegler-Nichols Tuning Rule: P

The Ziegler-Nichols tuning rules are shown in Table 12.4 on page 224 of the SEMD textbook. The proportional-only control, the control gain is set to 1/2 of the ultimate gain determined by experiment or from the Bode plot.

```

Kp = 0.5*Kcu;
displaytable(Kp, 'Kp');

K = tf([Kp],[1], 'TimeUnit', 'minutes');

% Closed-loop transfer functions

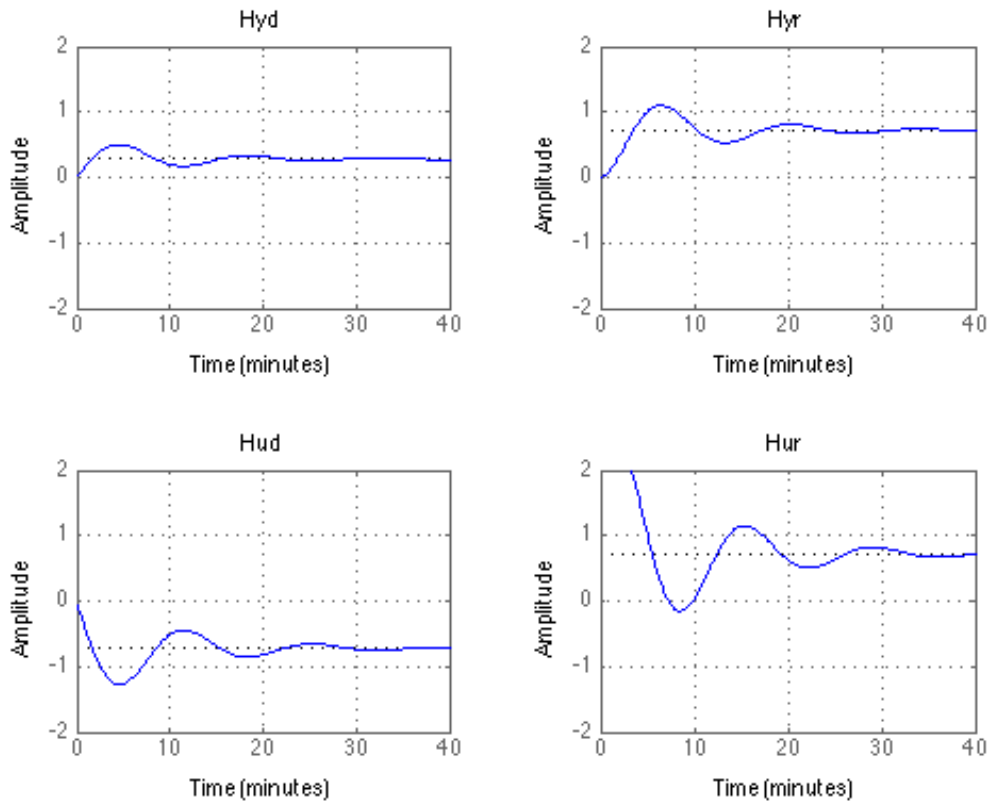
Hyd = Gd/(1 + Gp*Gv*K*Gm);
Hyr = Gp*Gv*K/(1 + Gp*Gv*K*Gm);
Hud = -K*Gd/(1 + K*Gm*Gp*Gv);
Hur = K/(1 + K*Gm*Gp*Gv);

```

% Plot Step Responses

```
t = 0:0.1:40;
ax = [min(t) max(t) -2 2];
subplot(2,2,1);step(Hyd,t);axis(ax);grid;title('Hyd');
subplot(2,2,2);step(Hyr,t);axis(ax);grid;title('Hyr');
subplot(2,2,3);step(Hud,t);axis(ax);grid;title('Hud');
subplot(2,2,4);step(Hur,t);axis(ax);grid;title('Hur');
```

Kp 2.5607



There are several problems with this proportional-only controller

- The step responses are underdamped
- Steady state offset is evident in the disturbance and setpoint responses.
- Significant control action is required for the setpoint response.

With proportional-only control there is an unfortunate tradeoff between damping and offset.

Ziegler-Nichols Tuning Rule: PI

Integral control eliminates offset. Ziegler-Nichols tuning rule (Table 12.4, page 224)

```
% Ultimate gain, crossover frequency, and ultimate period
```

```
[Kcu,~,wco] = margin(Gm*Gp*Gv);
```

```
Pu = 2*pi/wco;
```

```
% Ziegler-Nichols PI Tuning Rules
```

```
Kp = 0.45*Kcu;
```

```
Ti = Pu/1.2;
```

```
displaytable([Kp;Ti],{'Kp';'Ti'});
```

```
% PI Controller
```

```
P = Kp*tf([1],[1], 'TimeUnit', 'minutes');
```

```
I = Kp*tf([1],[Ti 0], 'TimeUnit', 'minutes');
```

```
K = P + I;
```

```
% Closed-loop transfer functions
```

```
Hyd = Gd/(1 + Gp*Gv*K*Km);
```

```
Hyr = Gp*Gv*K/(1 + Gp*Gv*K*Km);
```

```
Hud = -K*Gd/(1 + K*Km*Gp*Gv);
```

```
Hur = K/(1 + K*Km*Gp*Gv);
```

```
% Plot Step Responses
```

```
t = 0:0.1:40;
```

```
ax = [min(t) max(t) -2 2];
```

```
subplot(2,2,1);step(Hyd,t);axis(ax);grid;title('Hyd');
```

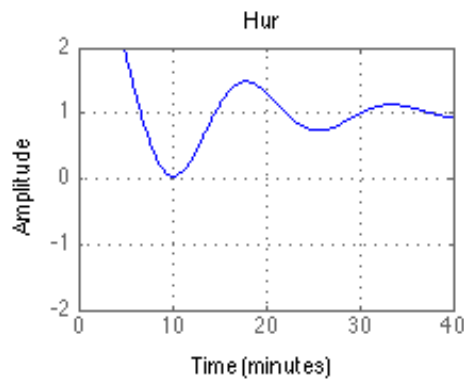
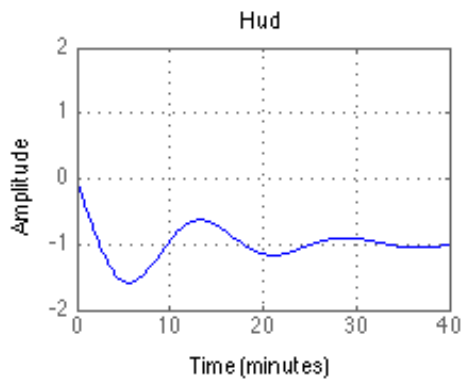
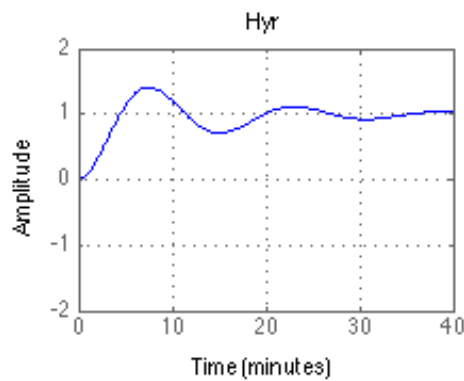
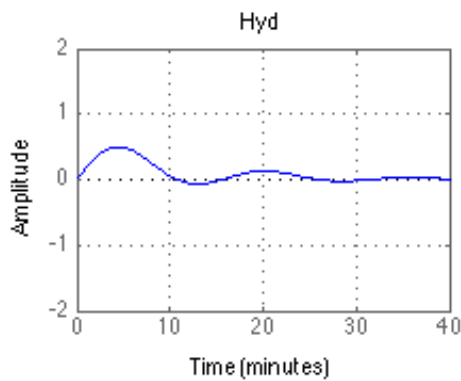
```
subplot(2,2,2);step(Hyr,t);axis(ax);grid;title('Hyr');
```

```
subplot(2,2,3);step(Hud,t);axis(ax);grid;title('Hud');
```

```
subplot(2,2,4);step(Hur,t);axis(ax);grid;title('Hur');
```

```
Kp 2.3047
```

```
Ti 9.3446
```



Observations

- Steady state offset is gone (due to integral action).
- Step responses are still underdamped.
- Significant control action is required for the setpoint response.

Take time to do a careful comparison. Try changing the control parameters to see what happens when you increase and decrease the integral time constant.

Ziegler-Nichols Tuning Rule: PID

Derivative action is used to increase damping. The increased damping also allows somewhat larger proportional control gains and shorter integral time constants. Ziegler-Nichols tuning rule (Table 12.4, page 224)

```
% Ultimate gain, crossover frequency, and ultimate period
```

```
[Kcu,~,wco] = margin(Gm*Gp*Gv);
Pu = 2*pi/wco;
```

```
% Ziegler-Nichols PID Tuning Rules
```

```
Kp = 0.6*Kcu;
Ti = Pu/2;
Td = Pu/8.0;
N= 10;
```

```
displaytable([Kp;Ti;Td;N],{'Kp';'Ti';'Td';'N'});
```



```

% PID Controller

P = Kp*tf([1],[1],'TimeUnit','minutes');
I = Kp*tf([1],[Ti 0],'TimeUnit','minutes');
D = Kp*tf([Td 0],[Td/N 1],'TimeUnit','minutes');

K = P + I + D;

% Closed-loop transfer functions

Hyd =      Gd/(1 + Gp*Gv*K*Gm);
Hyr = Gp*Gv*K/(1 + Gp*Gv*K*Gm);
Hud =  -K*Gd/(1 + K*Gm*Gp*Gv);
Hur =      K/(1 + K*Gm*Gp*Gv);

% Plot Step Responses

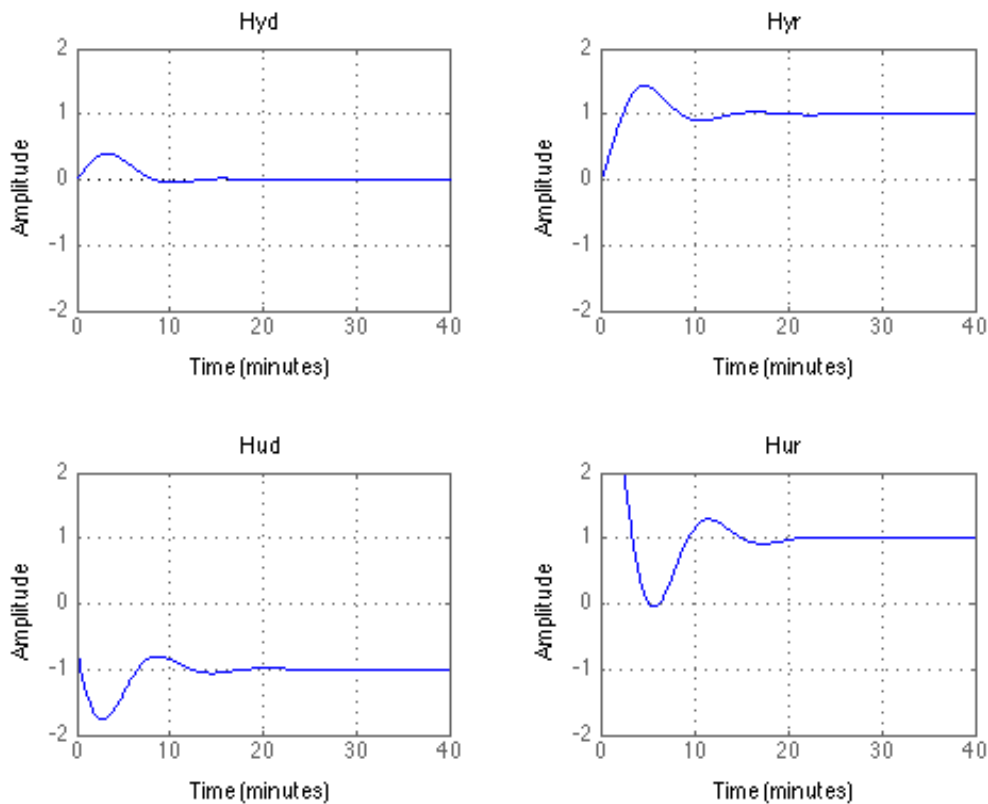
t = 0:0.1:40;
ax = [min(t) max(t) -2 2];
subplot(2,2,1);step(Hyd,t);axis(ax);grid;title('Hyd');
subplot(2,2,2);step(Hyr,t);axis(ax);grid;title('Hyr');
subplot(2,2,3);step(Hud,t);axis(ax);grid;title('Hud');
subplot(2,2,4);step(Hur,t);axis(ax);grid;title('Hur');

```

```

Kp  3.0729
Ti  5.6067
Td  1.4017
N    10

```



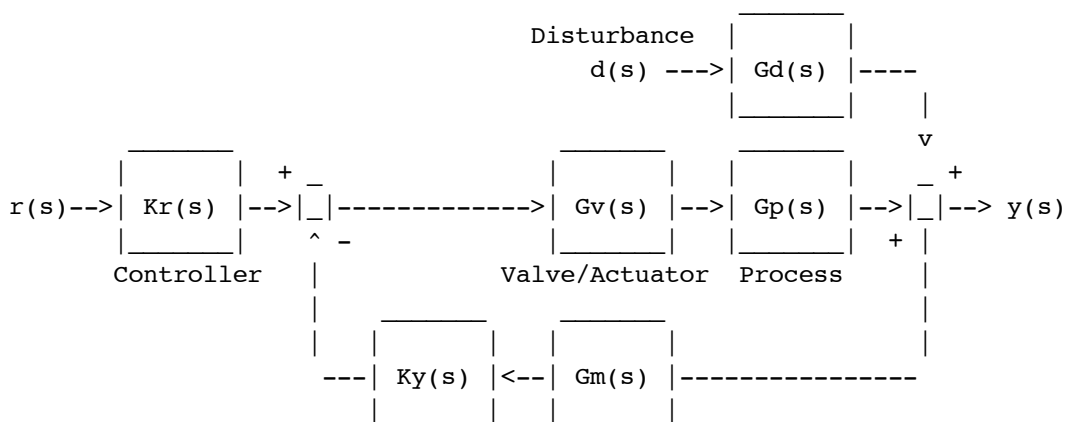
Observations

- Better tracking to steady state
- Better damping
- Significant control action is still required for the setpoint response.

Take time to do a careful comparison. Try changing the control parameters to see what happens when you increase and decrease the control parameters.

Two Degree of Freedom Controller

Further improvement in the closed-loop response is possible reconfigure the control loop to provide independent control of the disturbance rejection and setpoint response properties.



Two Parameter Control

```

% Ultimate gain, crossover frequency, and ultimate period

[Kcu,~,wco] = margin(Gm*Gp*Gv);
Pu = 2*pi/wco;

% Ziegler-Nichols PID Tuning Rules

Kp = 0.6*Kcu;
Ti = Pu/2.0;
Td = Pu/8.0;
N = 10;

displaytable([Kp;Ti;Td;N],{'Kp';'Ti';'Td';'N'});

% PID Control Parameters

P = Kp*tf([1],[1],'TimeUnit','minutes');
I = Kp*tf([1],[Ti 0],'TimeUnit','minutes');
D = Kp*tf([Td 0],[Td/N 1],'TimeUnit','minutes');

% Disturbance control Ky

Ky = P + I + D;

% Setpoint controller Kr

Kr = 0.0*P + I;

% Closed-loop transfer functions

Hyd = Gd/(1 + Gp*Gv*Ky*Gm);
Hyr = Gp*Gv*Kr/(1 + Gp*Gv*Ky*Gm);
Hud = -Ky*Gd/(1 + Ky*Gm*Gp*Gv);
Hur = Kr/(1 + Gp*Gv*Ky*Gm);

% Plot Step Responses

t = 0:0.1:40;
ax = [min(t) max(t) -2 2];
subplot(2,2,1);step(Hyd,t);axis(ax);grid;title('Hyd');
subplot(2,2,2);step(Hyr,t);axis(ax);grid;title('Hyr');
subplot(2,2,3);step(Hud,t);axis(ax);grid;title('Hud');
subplot(2,2,4);step(Hur,t);axis(ax);grid;title('Hur');

```

```

Kp 3.0729
Ti 5.6067
Td 1.4017
N 10

```

Observations

- The disturbance rejection properties are the same.
- Setpoint response is much better. Less overshoot with less control effort.

Closed Loop Transfer functions

Examine Bode plots for the closed-loop transfer functions. Can you see the relationships between these plots and the observed step responses?

```
figure(1);clf;  
bodeplot(Hyd,p);  
title('Hyd');  
  
figure(2);clf;  
bodeplot(Hyr,p);  
title('Hyr');
```

